

Density and Viscosity for Monoethanolamine + Water, + Ethanol, and + 2-Propanol

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Densities and viscosities were measured for monoethanolamine (MEA) + water, MEA + ethanol, and MEA + 2-propanol at 303.15, 313.15, and 323.15 K. The excess volumes and viscosity deviations from the mole fraction average were calculated and correlated by a Redlich–Kister type equation. McAllister's models were also applied to correlate the kinematic viscosities.

Introduction

Monoethanolamine (MEA) is a widely used agent in carbon dioxide and hydrogen sulfide removal processes. The viscosity of MEA is larger than that of conventional solvents such as water and lower alcohols by an order of magnitude. It is of interest to investigate the composition and temperature effects on volumetric and transport properties of the mixtures containing MEA and these conventional solvents. This paper reports density, viscosity, and kinematic viscosity data for binary systems of MEA + water, MEA + ethanol, and MEA + 2-propanol at atmospheric pressure (nominal value 0.1 MPa) and temperatures from 303.15 to 323.15 K over the entire composition range. No data are available in the literature for these mixtures at comparable conditions.

Experimental Section

Monoethanolamine (99 mass %) was purchased from Janssen Chimica, ethanol (99.8 mass %) from Ferak, and 2-propanol (99.5 mass %) from Aldrich. The purity of the chemicals was checked by gas chromatography analysis. No impurity peak was detected. All these compounds were used without further purification. Deionized distilled water, conductivity better than $2 \times 10^{-6} \Omega^{-1} \times \text{cm}^{-1}$, was prepared in our laboratory.

Pycnometers and a Haake falling-ball viscometer were employed to measure density and viscosity, respectively. To prevent the viscometer from being corroded by MEA, the metal surfaces in contact with the sample were gold plated. The detailed experimental procedure has been described elsewhere (1). In general, the accuracy of the measurements is estimated to be $\pm 0.1\%$ for density, $\pm 1.5\%$ for viscosity, ± 0.1 K for temperature, and ± 0.0004 in mole fraction for mixture preparation. The following equation converts falling time (t) into viscosity (η):

$$\eta = K(\rho_b - \rho)t \quad (1)$$

where ρ_b is the density of the ball and, ρ is the density of the liquid determined at the measuring temperature. The ball constant K was determined from the falling-time measurements with the literature viscosity values of 1-butanol at 307.69 K, 2-methyl-2-propanol at 313.15 K (2), methanol + water at 283.15 K, 1-propanol + water at 303.15 K (3), and MEA at 298.15 K (4) and 313.15 K (5) and expressed as a function of liquid density over a density

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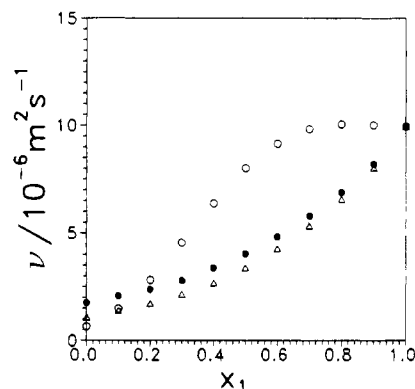


Figure 1. Kinematic viscosities at 313.15 K: (○) MEA (1) + water (2); (△) MEA (1) + ethanol (2); (●) MEA (1) + 2-propanol (2).

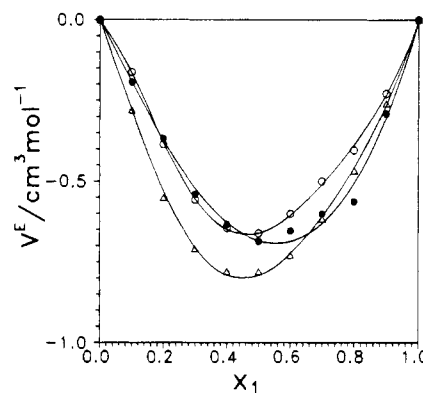


Figure 2. Excess volumes at 313.15 K: (○) MEA (1) + water (2); (△) MEA (1) + ethanol (2); (●) MEA (1) + 2-propanol (2); (---) calculated from eq 6.

range of $0.7632\text{--}1.002 \text{ g}\cdot\text{cm}^{-3}$.

$$K = 0.05226 + 0.003062(\rho/(\text{g}\cdot\text{cm}^{-3})) \quad (2)$$

The average absolute deviation (AAD) of the above correlation is 0.80%, and the maximum deviation is -1.26% by comparing with the literature data.

Results and Discussion

The observed densities (ρ) and viscosities (η) for the pure components are compared with literature values in Table 1, which shows that the measurements agree with literature values within the experimental errors. Tables 2–4 list the experimental results of MEA + water, MEA + ethanol, and MEA + 2-propanol, respectively. Figure 1

Table 1. Comparison of Density and Viscosity of Pure Components from This Work with the Literature Values

compd	T/K	$\rho/(\text{gcm}^{-3})$		$\eta/(\text{mPa}\cdot\text{s})$	
		this work	lit.	this work	lit.
monoethanolamine	303.15	1.009	1.008 (5) 1.00889 (6)	15.0	15.1 (5)
	313.15	0.9999	1.000 (5) 1.00020 (6)	9.94	10.0 (5)
	323.15	0.9918	0.9924 (5) 0.99179 (6)	6.87	6.97 (5)
water	303.15	0.9957	0.9957 (7) 0.99565 (6)	0.800	0.7975 (8) 0.7966 (6) 0.8005 (3) 0.7971 (9) 0.802 (10)
	313.15	0.9923	0.9923 (7) 0.99219 (6)	0.655	0.6530 (8) 0.6521 (6) 0.6568 (3) 0.6531 (9) 0.656 (10)
	323.15	0.9881	0.9981 (7) 0.98804 (6)	0.549	0.5469 (8) 0.5463 (6) 0.5514 (3) 0.5441 (9) 0.555 (10)
ethanol	303.15	0.7807	0.7808 (6)	0.990	0.987 (6) 0.9817 (11) 0.994 (12) 0.990 (13) 1.000 (14) 0.999 (3)
	313.15	0.7722	0.7721 (6)	0.834	0.826 (6) 0.835 (15) 0.834 (14) 0.833 (3)
	323.15	0.7635	0.7636 (6)	0.701	0.696 (6) 0.702 (3) 0.702 (14) 0.702 (15)
2-propanol	303.15	0.7768	0.7770 (6)	1.78	1.767 (6) 1.791 (14) 1.783 (13)
	313.15	0.7680	0.7683 (6)	1.35	1.340 (6) 1.358 (9)
	323.15	0.7593	0.7593 (6)	1.04	1.033 (6) 1.045 (9)

Table 2. Density (ρ), Viscosity (η), and Kinematic Viscosity (ν) for Monoethanolamine (1) + Water (2)

x_1	303.15 K			313.15 K			323.15 K		
	$\rho/(\text{gcm}^{-3})$	$\eta/(\text{mPa}\cdot\text{s})$	$\nu/(10^{-6} \text{ m}^2\cdot\text{s}^{-1})$	$\rho/(\text{gcm}^{-3})$	$\eta/(\text{mPa}\cdot\text{s})$	$\nu/(10^{-6} \text{ m}^2\cdot\text{s}^{-1})$	$\rho/(\text{gcm}^{-3})$	$\eta/(\text{mPa}\cdot\text{s})$	$\nu/(10^{-6} \text{ m}^2\cdot\text{s}^{-1})$
0.1000	1.007	1.91	1.90	1.002	1.48	1.48	0.9972	1.21	1.21
0.2000	1.017	3.87	3.81	1.010	2.84	2.81	1.004	2.16	2.15
0.3000	1.021	6.67	6.53	1.015	4.62	4.55	1.008	3.36	3.33
0.4000	1.024	9.68	9.45	1.016	6.48	6.38	1.009	4.62	4.58
0.5000	1.023	12.3	12.0	1.015	8.13	8.01	1.008	5.65	5.61
0.6000	1.020	14.0	13.7	1.013	9.26	9.14	1.005	6.38	6.35
0.7000	1.018	15.2	14.9	1.010	9.92	9.82	1.002	6.84	6.83
0.8000	1.015	15.4	15.2	1.007	10.1	10.0	0.9992	6.94	6.95
0.9000	1.012	15.3	15.1	1.004	10.0	9.96	0.9961	6.93	6.96

Table 3. Density (ρ), Viscosity (η), and Kinematic Viscosity (ν) for Monoethanolamine (1) + Ethanol (2)

x_1	303.15 K			313.15 K			323.15 K		
	$\rho/(\text{gcm}^{-3})$	$\eta/(\text{mPa}\cdot\text{s})$	$\nu/(10^{-6} \text{ m}^2\cdot\text{s}^{-1})$	$\rho/(\text{gcm}^{-3})$	$\eta/(\text{mPa}\cdot\text{s})$	$\nu/(10^{-6} \text{ m}^2\cdot\text{s}^{-1})$	$\rho/(\text{gcm}^{-3})$	$\eta/(\text{mPa}\cdot\text{s})$	$\nu/(10^{-6} \text{ m}^2\cdot\text{s}^{-1})$
0.1000	0.8080	1.33	1.65	0.7992	1.11	1.39	0.7900	0.967	1.22
0.2000	0.8345	1.73	2.07	0.8262	1.42	1.72	0.8174	1.19	1.46
0.8000	0.8600	2.30	2.67	0.8517	1.83	2.15	0.8430	1.47	1.74
0.4000	0.8844	3.05	3.45	0.8759	2.34	2.67	0.8670	1.85	2.13
0.5000	0.9077	3.96	4.36	0.8990	3.05	3.39	0.8900	2.34	2.63
0.6000	0.9296	5.37	5.78	0.9212	3.93	4.27	0.9123	2.95	3.23
0.7000	0.9505	7.03	7.40	0.9423	5.03	5.34	0.9338	3.70	3.96
0.8000	0.9705	9.05	9.33	0.9626	6.32	6.57	0.9541	4.54	4.76
0.9000	0.9898	11.6	11.7	0.9818	7.87	8.02	0.9735	5.57	5.72

illustrates the kinematic viscosities ($\nu = \eta/\rho$) of these three binary solutions varying with composition at 313.15 K. For the aqueous system, the viscosity increases markedly with the mole fraction of MEA (x_1), reaches a weak maximum

at about $x_1 = 0.8$, and then decreases slightly to the value of pure MEA. Unlike the aqueous system, the viscosities of alcohol-containing mixtures increase monotonically with the mole fraction of MEA. The excess volume (V^E) was

Table 4. Density (ρ), Viscosity (η), and Kinematic Viscosity (ν) for Monoethanolamine (1) + 2-Propanol (2)

x_1	303.15 K			313.15 K			323.15 K		
	$\rho/(\text{g}\cdot\text{cm}^{-3})$	$\eta/(\text{mPa}\cdot\text{s})$	$\nu/(10^{-6} \text{ m}^2\cdot\text{s}^{-1})$	$\rho/(\text{g}\cdot\text{cm}^{-3})$	$\eta/(\text{mPa}\cdot\text{s})$	$\nu/(10^{-6} \text{ m}^2\cdot\text{s}^{-1})$	$\rho/(\text{g}\cdot\text{cm}^{-3})$	$\eta/(\text{mPa}\cdot\text{s})$	$\nu/(10^{-6} \text{ m}^2\cdot\text{s}^{-1})$
0.1011	0.7972	2.11	2.65	0.7884	1.63	2.07	0.7794	1.27	1.63
0.2002	0.8181	2.53	3.09	0.8093	1.92	2.37	0.8004	1.49	1.86
0.3001	0.8403	3.08	3.67	0.8315	2.31	2.78	0.8228	1.78	2.16
0.4003	0.8623	3.86	4.48	0.8541	2.88	3.37	0.8452	2.21	2.61
0.5001	0.8860	4.90	5.53	0.8773	3.55	4.05	0.8687	2.65	3.05
0.5999	0.9090	6.12	6.73	0.9007	4.35	4.83	0.8924	3.22	3.61
0.7001	0.9337	7.70	8.25	0.9252	5.37	5.80	0.9169	3.89	4.24
0.8000	0.9582	9.55	9.97	0.9512	6.54	6.88	0.9421	4.69	4.98
0.9000	0.9839	11.9	1.21	0.9751	7.97	8.17	0.9671	5.64	5.83

Table 5. Coefficients of Eq 6

mixture	T/K	A_0	A_1	A_2	A_3	AAD ^a /%
MEA + water	303.15	-2.5962	0.6670	0.9623	-1.2220	0.02
	313.15	-2.6417	0.5192	0.6854	-1.5542	0.01
	323.15	-2.6109	0.4010	0.3067	-1.3942	0.01
MEA + ethanol	303.15	-2.9975	0.6109	0.4261	0.0117	0.00
	313.15	-3.1583	0.6958	0.2359	-0.9169	0.01
	323.15	-3.1914	0.8971	0.4217	-1.4779	0.03
MEA + 2-propanol	303.15	-2.1544	-0.1155	-0.0698	-0.8473	0.02
	313.15	-2.7368	-0.6094	-0.0364	-0.2580	0.03
	323.15	-2.4599	-0.4765	1.5985	-0.8996	0.01

$$^a \text{AAD} = (100/n) \sum_{k=1}^n |e_k^{\text{cal}} - e_k^{\text{exp}}| / e_k^{\text{exp}}$$

Table 6. Coefficients of Eq 7

mixture	T/K	B_0	B_1	B_2	B_3	AAD ^a /%
MEA + water	303.15	16.9447	17.3791	-15.3004	-5.4789	1.08
	313.15	11.0221	9.8989	-9.3797	-3.0882	0.64
	323.15	7.6099	5.7710	-5.8297	-1.7287	0.68
MEA + ethanol	303.15	-15.7096	-4.6399	-2.1424	-3.2077	0.93
	313.15	-9.2627	-2.2000	-0.9187	-2.2382	0.53
	323.15	-5.7585	-1.2236	0.0382	-1.6695	0.22
MEA + 2-propanol	303.15	-13.9995	-3.6520	-2.2402	-3.0370	0.30
	313.15	-8.3692	-1.9261	-1.5537	-2.5882	0.27
	323.15	-5.1931	-1.1325	-0.5921	-1.3493	0.42

$$^a \text{AAD} = (100/n) \sum_{k=1}^n |n_k^{\text{cal}} - n_k^{\text{exp}}| / n_k^{\text{exp}}$$

Table 7. Coefficients of McAllister's Models

mixture	T/K	three-body model			four-body model			AAD ^a /%
		ν_{12}	ν_{21}	AAD ^a /%	ν_{1112}	ν_{1122}	ν_{2221}	
MEA + water	303.15	15.4285	25.012	0.65	15.1034	19.5929	10.1246	0.62
	313.15	10.0327	16.0719	0.37	10.1889	11.8967	7.2443	0.17
	323.15	6.9091	10.9906	0.82	7.1227	7.7867	5.3617	0.32
MEA + ethanol	303.15	7.0466	2.8598	0.74	8.4519	4.5258	2.3188	0.73
	313.15	5.1096	2.3199	0.75	6.0572	3.3938	1.9418	0.73
	323.15	3.7546	1.9289	1.34	4.5072	2.4433	1.7565	1.20
MEA + 2-propanol	303.15	8.1025	3.5256	0.71	8.7621	5.9872	2.9915	0.60
	313.15	5.5486	2.8474	0.80	6.0780	4.3047	2.3899	0.51
	323.15	4.0207	2.3041	0.81	4.4385	3.2817	1.9134	0.64

$$^a \text{AAD} = (100/n) \sum_{k=1}^n |v_k^{\text{cal}} - v_k^{\text{exp}}| / v_k^{\text{exp}}$$

calculated from the density data by

$$V^{\text{E}} = V - (x_1 V_1 + x_2 V_2) \quad (3)$$

with

$$V = (x_1 M_1 + x_2 M_2) / \rho \quad (4)$$

where V is the molar volume of the mixture and V_1 , M_1 , V_2 , and M_2 are the molar volumes and molecular weights of components 1 and 2, respectively. The viscosity deviation from a mole fraction average ($\delta\eta$) is given by

$$\delta\eta = \eta - (x_1 \eta_1 + x_2 \eta_2) \quad (5)$$

where η_1 and η_2 are the viscosities of pure components 1 and 2, respectively. Figure 2 presents the excess volumes

at 313.15 K, indicating negative volume changes of mixing for those three systems. The volume contraction in MEA + ethanol is slightly greater than those in MEA + 2-propanol and MEA + water. The comparison of viscosity deviations is made as shown in Figure 3. It reveals a positive deviation for MEA + water except in the range of low MEA concentrations and a negative deviation for the alcohol-containing systems over the entire composition range.

The isothermal excess volumes and viscosity deviations were correlated by a Redlich-Kister type equation:

$$V^{\text{E}}/(\text{cm}^3 \cdot \text{mol}^{-1}) = x_1 x_2 \sum_{k=0}^3 A_k (x_1 - x_2)^k \quad (6)$$

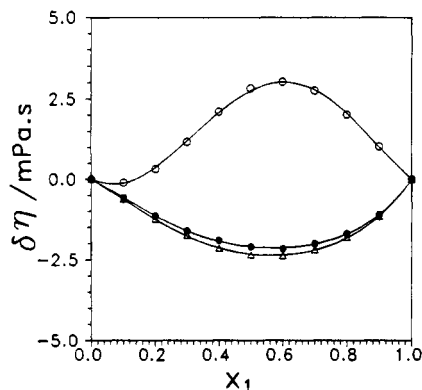


Figure 3. Viscosity deviations at 313.15 K: (O) MEA (1) + water (2); (Δ) MEA (1) + ethanol (2); (\bullet) MEA (1) + 2-propanol (2); (—) calculated from eq 7.

$$\delta\eta/(\text{mPa}\cdot\text{s}) = x_1x_2 \sum_{k=0}^3 B_k(x_1 - x_2)^k \quad (7)$$

The coefficients of A_k and B_k were obtained by fitting the equations to the experimental values with a least-squares algorithm. Tables 5 and 6 give the coefficients together with the AAD of the calculated density and viscosity.

McAllister's multibody interaction model (16) is widely used for correlating the kinematic viscosity of liquid mixtures. The three-body model is defined as

$$\ln \nu = x_1^3 \ln \nu_1 + 3x_1^2x_2 \ln \nu_{12} + 3x_1x_2^2 \ln \nu_{21} + x_2^3 \ln \nu_2 - \ln[x_1 + x_2(M_2/M_1)] + 3x_1^2x_2 \ln[(2 + M_2/M_1)/3] + 3x_1x_2^2 \ln[(1 + 2M_2/M_1)/3] + x_2^3 \ln(M_2/M_1) \quad (8)$$

and the four-body model is given by

$$\ln \nu = x_1^4 \ln \nu_1 + 4x_1^3x_2 \ln \nu_{1112} + 6x_1^2x_2^2 \ln \nu_{1122} + 4x_1x_2^3 \ln \nu_{2221} + x_2^4 \ln \nu_2 - \ln[x_1 + x_2(M_2/M_1)] + 4x_1^3x_2 \ln[(3 + M_2/M_1)/4] + 6x_1^2x_2^2 \ln[(1 + M_2/M_1)/2] + 4x_1x_2^3 \ln[(1 + 3M_2/M_1)/4] + x_2^4 \ln(M_2/M_1) \quad (9)$$

where ν_{12} , ν_{21} , ν_{1112} , ν_{1122} , and ν_{2221} are the model param-

eters. Table 7 reports the calculated results. It shows that the three-body model is adequate enough for those three MEA-containing systems.

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